

Table 1: Comparison of strain capability [4, 5, 6 and 20]

Material	Saturation strain in [ppm]	Curie temperature in [K]
Ni	-50	630
Fe	-14	1040
Fe ₃ O ₄	60	860
Terfenol-D	2000	650
Tb _{0.5} Zn _{0.5}	5500	180
Tb _{0.5} Dy _x Zn	5000	200

Table 2: Typical layouts in comparison similar to [7, 8]

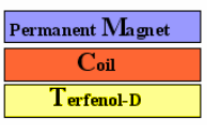
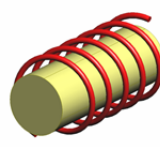
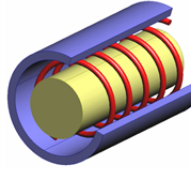
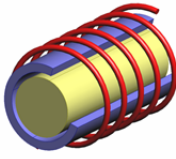
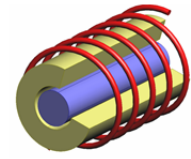
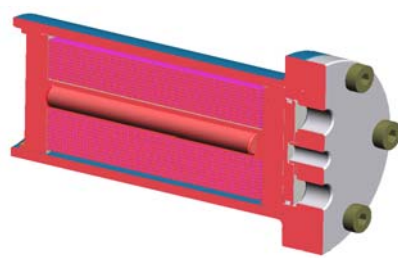
Actuator Layout	TC	TCM	TMC	MTC
				
<i>Typical actuator features</i>				
Magnetic bias with	DC coil	Permanent magnets		
Magnetic bias level	Low	Medium	Medium, high	High
Terfenol-D shape	Rod, bar	Rod	Rod	Hollow rod
Structure	Simple	Medium	Medium	Complex
Field inhomogeneity	Low	Low	Medium	High

Table 3: “MS”-actuator key data

“MS”-actuator, 3D CAD cut view	Actuator key data	Experimental results
	Actuator coil: -950 turns, 1.5Ohm -wire diameter of 1.12mm Terfenol-D shaft: -shaft diameter of 8mm -shaft length 67.5mm	Optimized pre-stress: 12MPa (600N pre-load) Strain capability: 0.065mm @ 10 A (1000ppm @ 105 kA/m) Blocked force: > 4500N

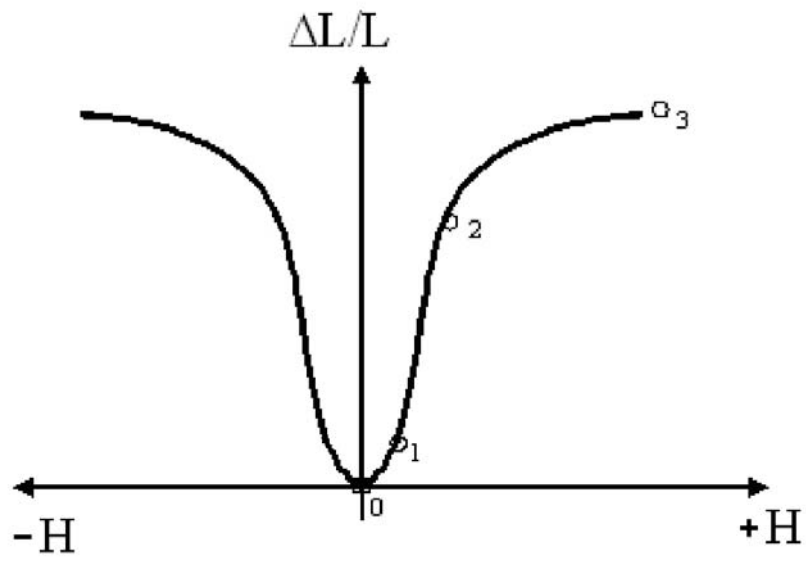


Fig.1: Strain versus magnetic field

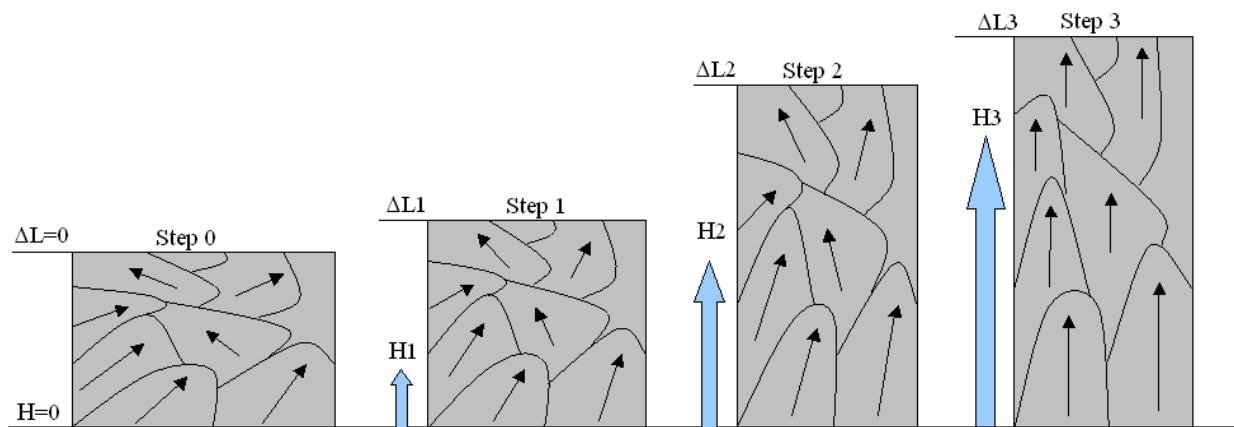


Fig. 2: "MS"-effect, schematically

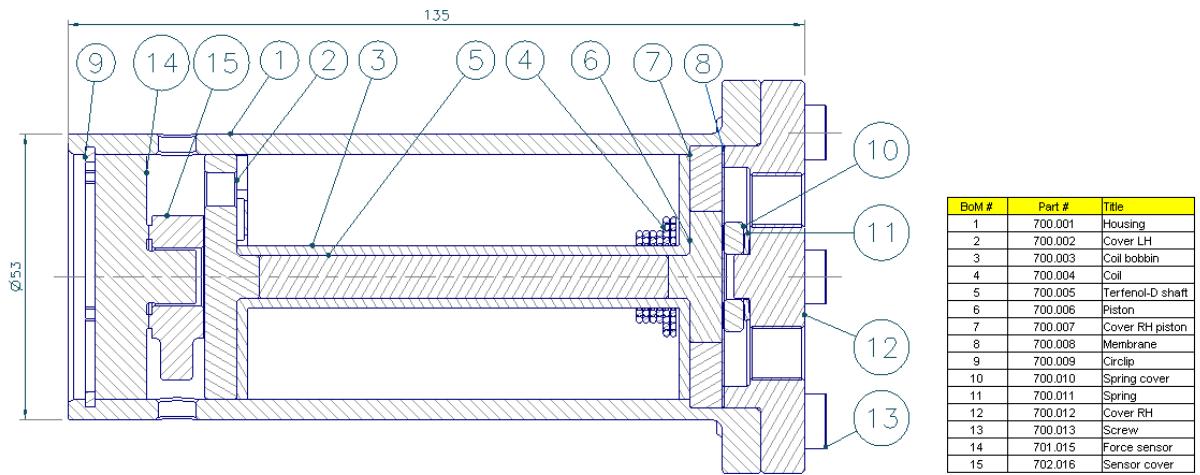


Fig. 3: Cross-section of the actuator used in the study

TERFENOL-D PHYSICAL PROPERTIES	
Nominal Composition	Tb _{0.3} Dy _{0.7} Fe _{1.92}
Mechanical Properties	
Young's Modulus	25-35 GPA
Sound Speed	1640-1940 m/s
Tensile Strength	28 Mpa
Compressive Strength	700 Mpa
Thermal Properties	
Coefficient of Thermal Expansion	12ppm/°C
Specific Heat	0.35kJ/kg-K
Thermal Conductivity	13.5 W/m-k
Electrical Properties	
Resistivity	58 x 10 ⁻⁸ Ω-m
Curie Temperature	380 °C
Magnetostrictive Properties	
Strain (estimated linear)	800-1200ppm
Energy Density	14-25 kJ/ m ³
Magnetomechanical Properties	
Relative Permeability	3-10
Coupling Factor	0.75

Fig. 4: Supplier characteristic and specification for Terfenol-D shaft [4]

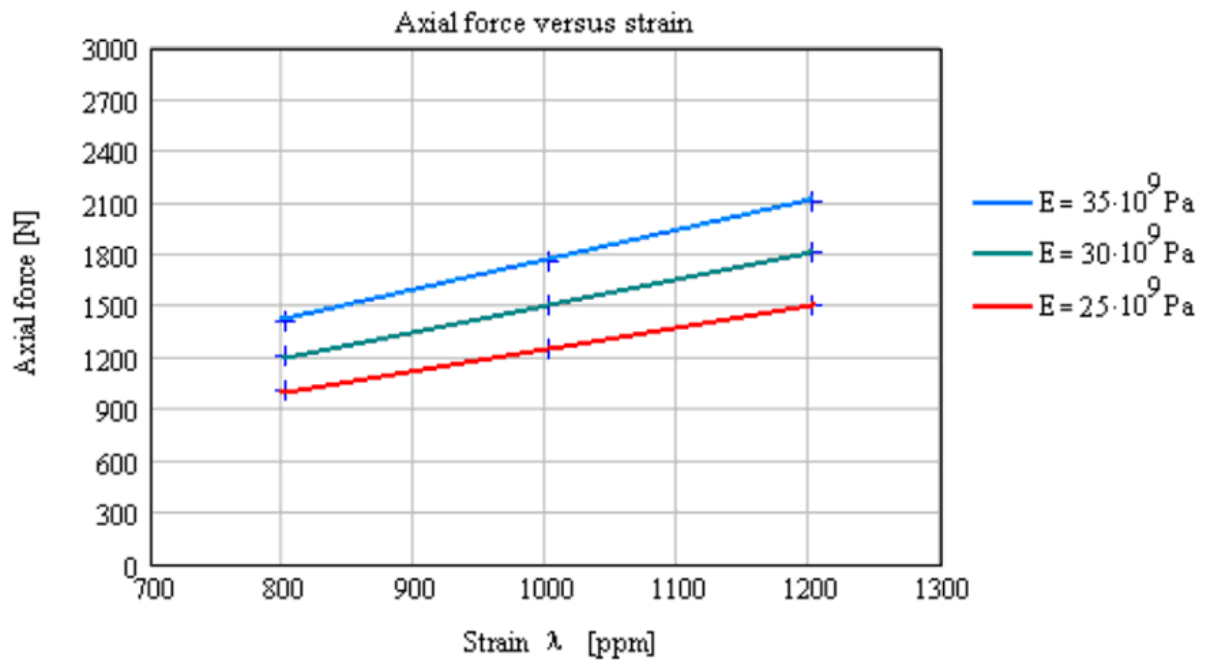


Fig. 5: Axial force versus strain and Young's modulus E as parameter

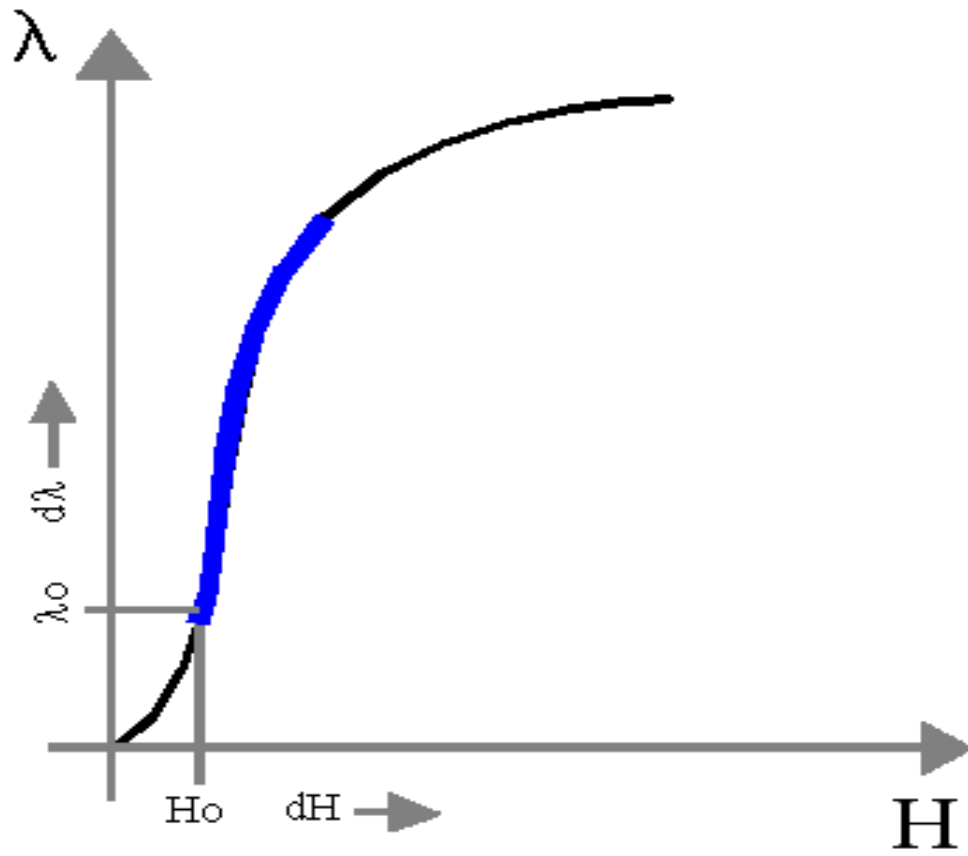


Fig.6: Typical optimization with magnetic bias

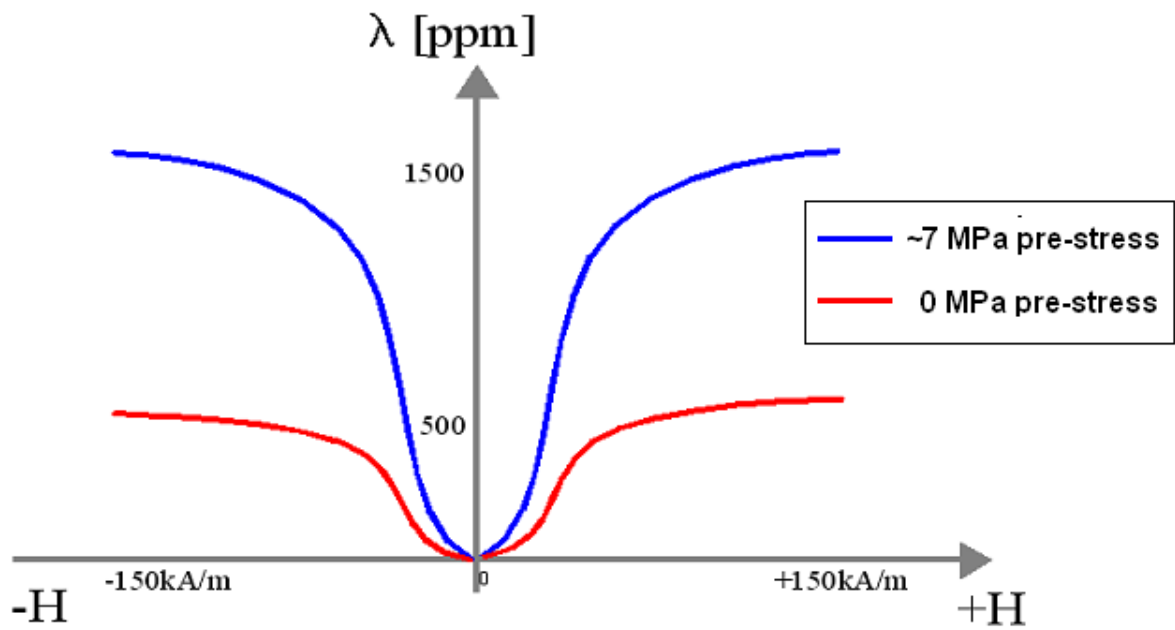


Fig.7: Typical optimization with mechanic bias [similar to 9, 10 and 11]

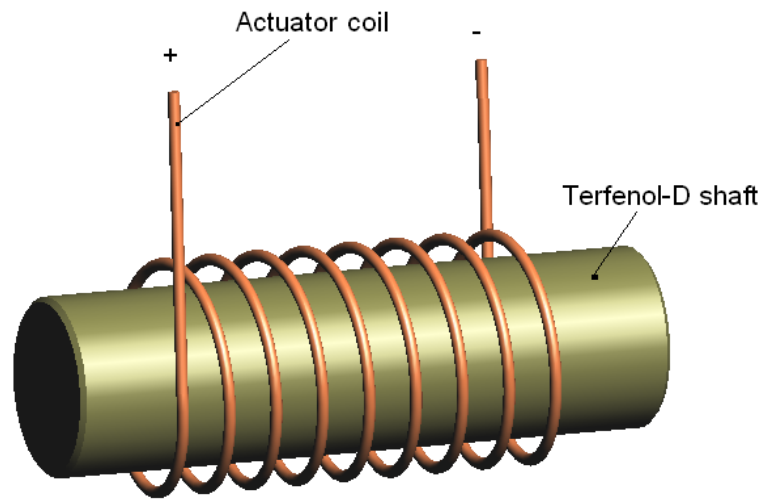


Fig. 8: TC-Layout of the actuator coil

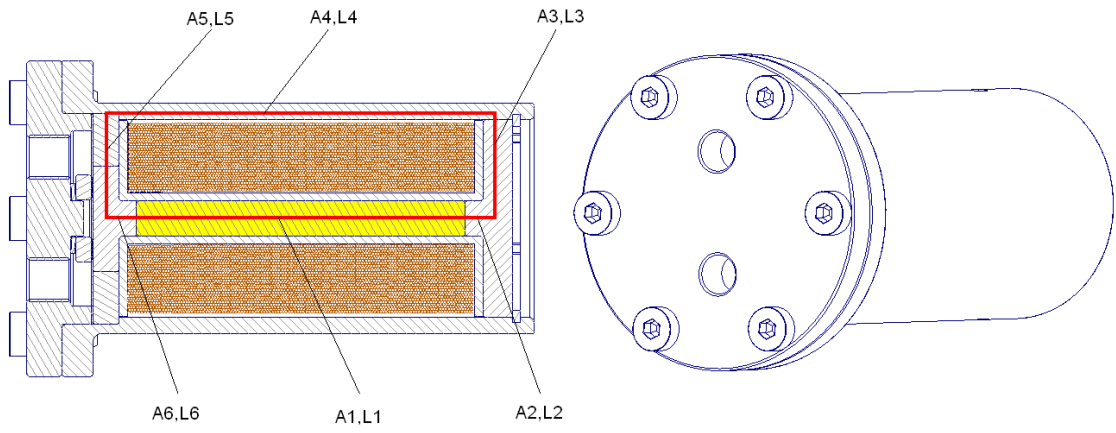


Fig. 9: Magnetic path through the actuator

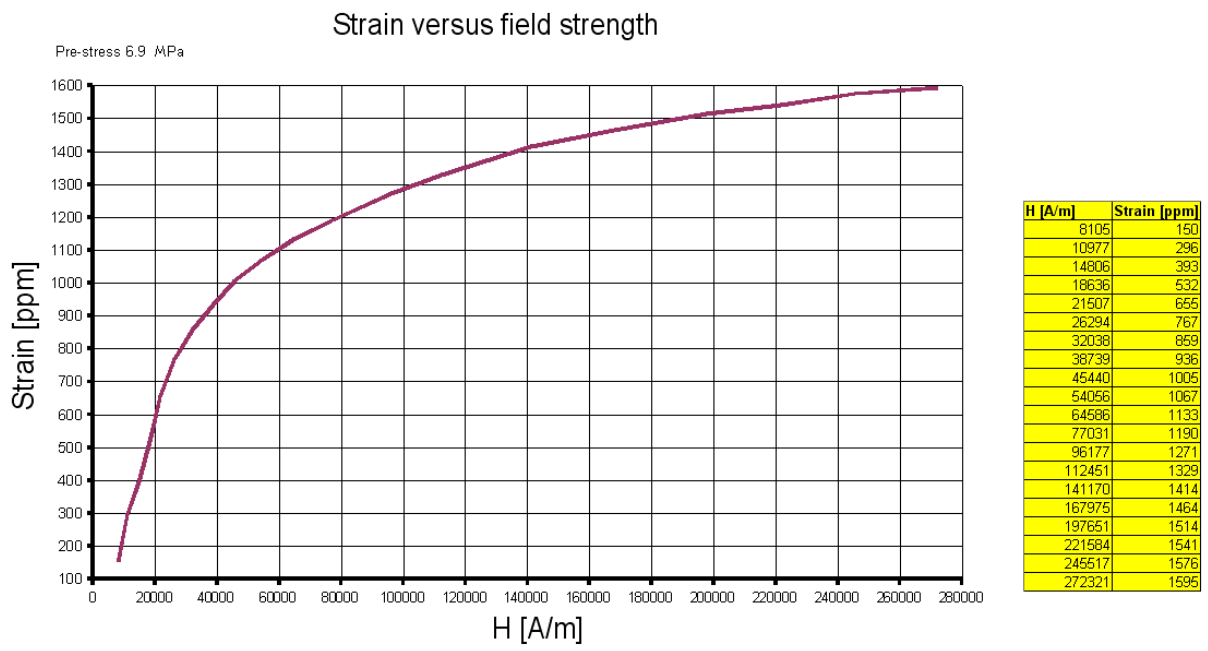
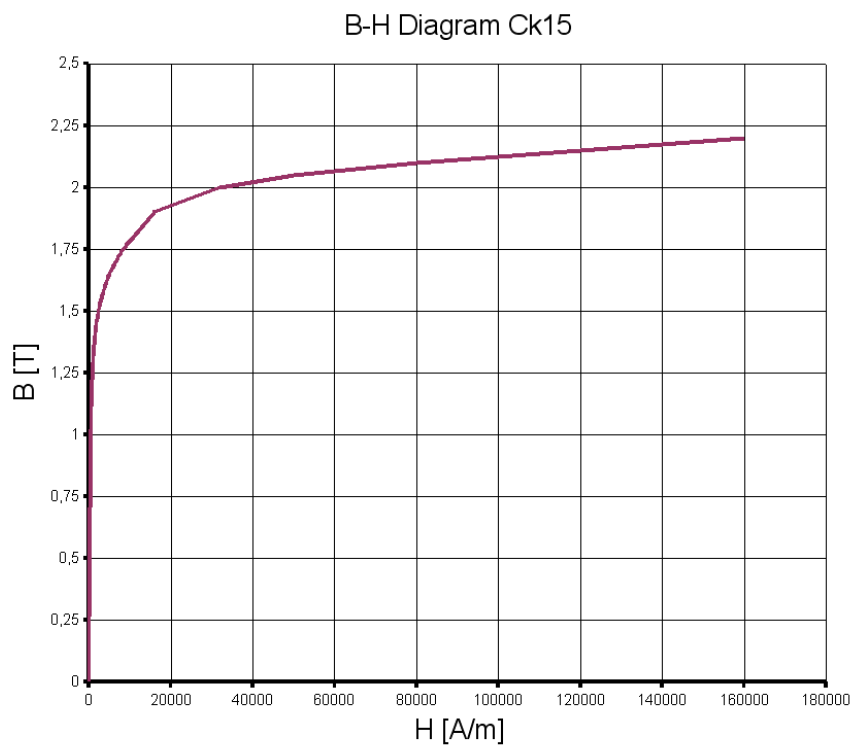


Fig. 10: Strain versus applied magnetic field intensity (A/m) [4]



H	B	μ	μ_r
0	0	-	-
100	0,26	2,62E-003	2087
200	0,5	2,48E-003	1976
300	0,7	2,35E-003	1868
400	0,89	2,21E-003	1763
500	1,02	2,04E-003	1624
600	1,11	1,86E-003	1476
700	1,17	1,68E-003	1336
800	1,22	1,53E-003	1215
900	1,26	1,40E-003	1112
1000	1,29	1,29E-003	1026
1100	1,32	1,20E-003	952
1200	1,34	1,12E-003	889
1300	1,36	1,05E-003	834
1400	1,38	9,86E-004	785
1500	1,4	9,32E-004	742
1600	1,41	8,84E-004	703
1700	1,43	8,40E-004	669
1800	1,44	8,01E-004	637
1900	1,45	7,65E-004	609
2000	1,47	7,33E-004	583
2400	1,5	6,27E-004	499
2800	1,54	5,49E-004	436
3200	1,56	4,88E-004	388
3600	1,59	4,40E-004	350
4000	1,61	4,01E-004	319
4400	1,62	3,69E-004	294
4800	1,64	3,42E-004	272
5200	1,66	3,18E-004	253
5600	1,67	2,98E-004	237
6000	1,68	2,80E-004	223
6400	1,7	2,65E-004	211
6800	1,71	2,51E-004	200
7200	1,72	2,39E-004	190
7600	1,73	2,28E-004	181
8000	1,74	2,17E-004	173
8400	1,75	2,08E-004	166
8800	1,76	2,00E-004	159
9200	1,77	1,92E-004	153
9600	1,78	1,85E-004	147
16000	1,9	1,19E-004	95
32000	2	6,25E-005	50
50000	2,05	4,10E-005	33
80000	2,1	2,63E-005	21
160000	2,2	1,38E-005	11

Fig. 11: B-H diagram of Ck15 with measurement data

B-H Diagram Terfenol-D (7.2MPa)

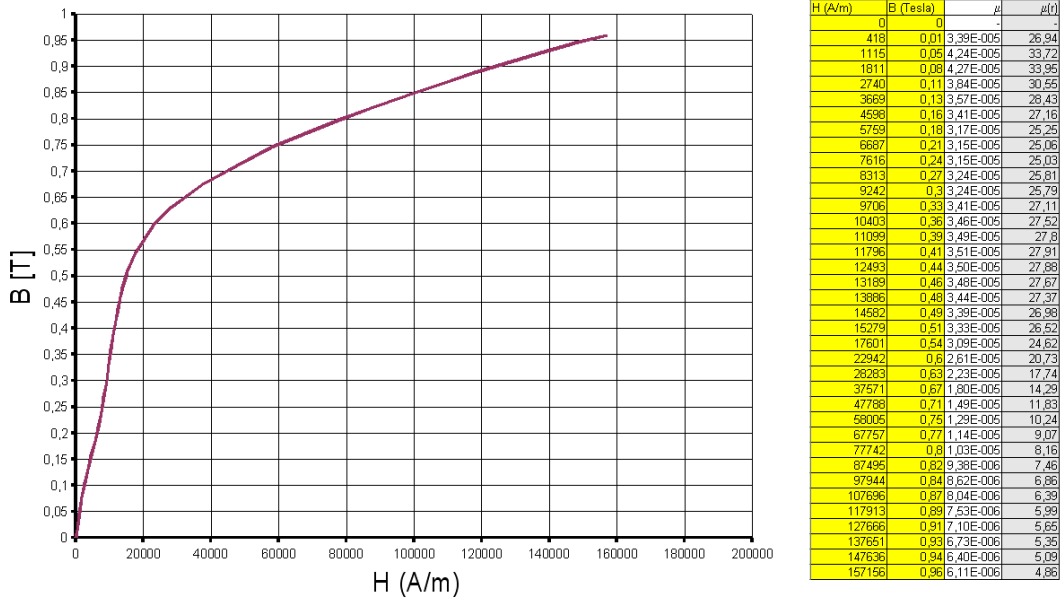
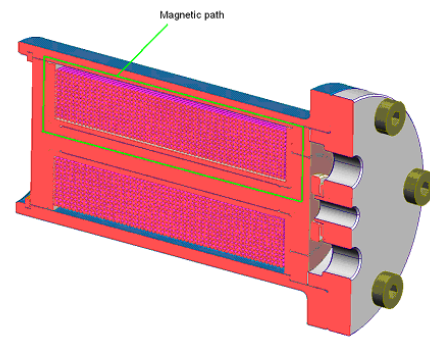
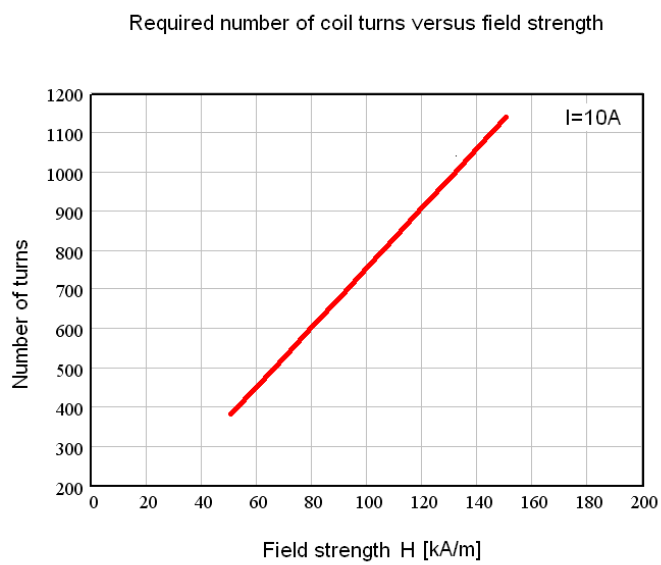


Fig. 12: B-H diagram of Terfenol-D with measurement data [4]



Calculation parameter
 Geometry: assembly 700.000
 Relative permeability:
 Ck15 635 (average for up to 160kA/m)
 Terfenol-D 20 (average up up to 160kA/m)

Fig. 13: Number of turns versus achievable magnetic field strength

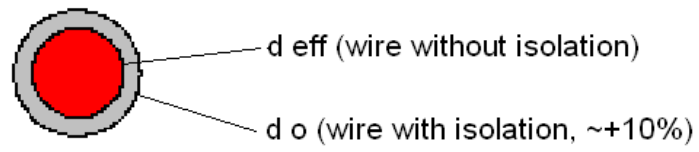
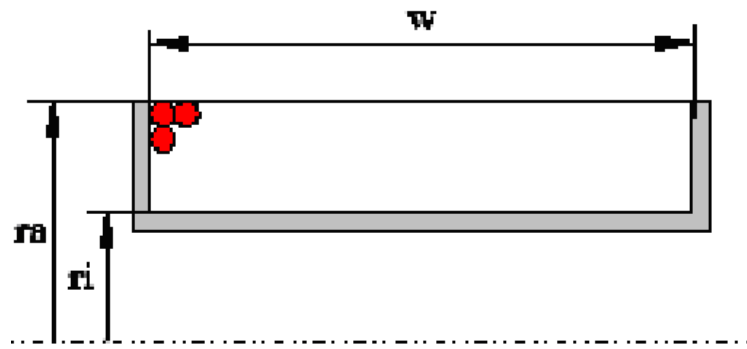


Fig. 14: Air coil geometry

Current density versus wire diameter

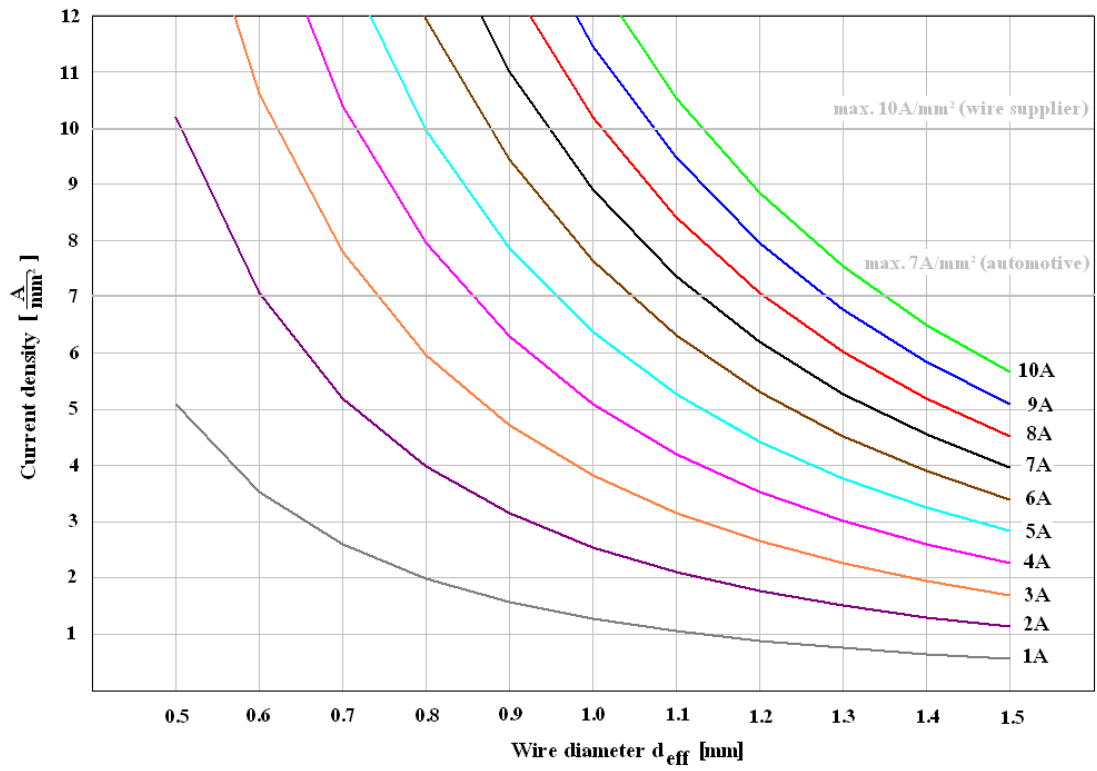
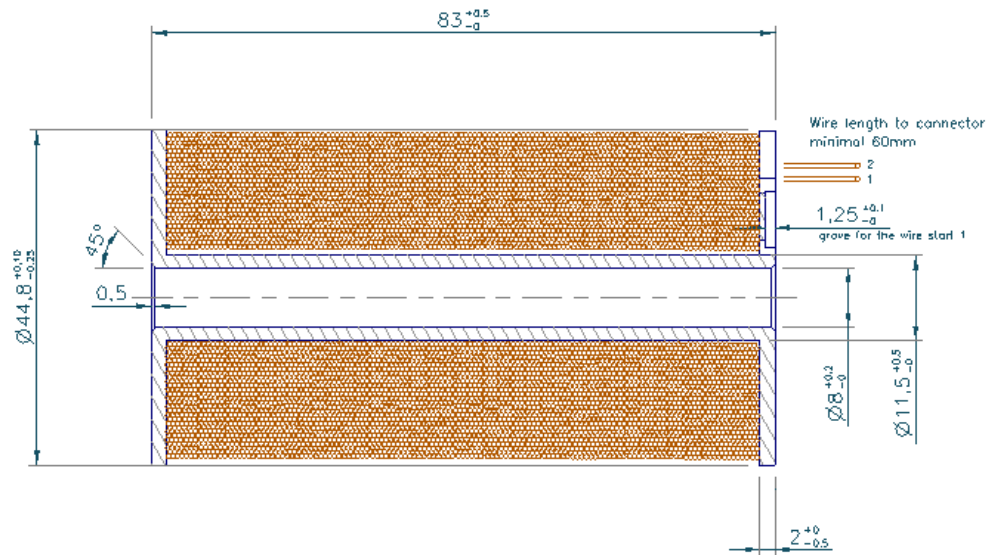


Fig. 15: Current density versus wire diameter with current as parameter



Actuator coil for rig tests
 Temperature range: -20 C up to $+120$ C
 Supplied voltage: $12V \pm 3V$,
 Frequency: 0 Hz at DC and 1000 Hz at AC
 Resistance at R_t : >1.52 Ohm at DC
 Inductance: 23 mH
 Nominal current: <9.8 A
 Number of turns: >1000
 Wire material: Copper
 Wire bare diameter: 1.15 mm (AWG17)

Fig. 16: Geometry and coil specification of the magnetostrictive actuator

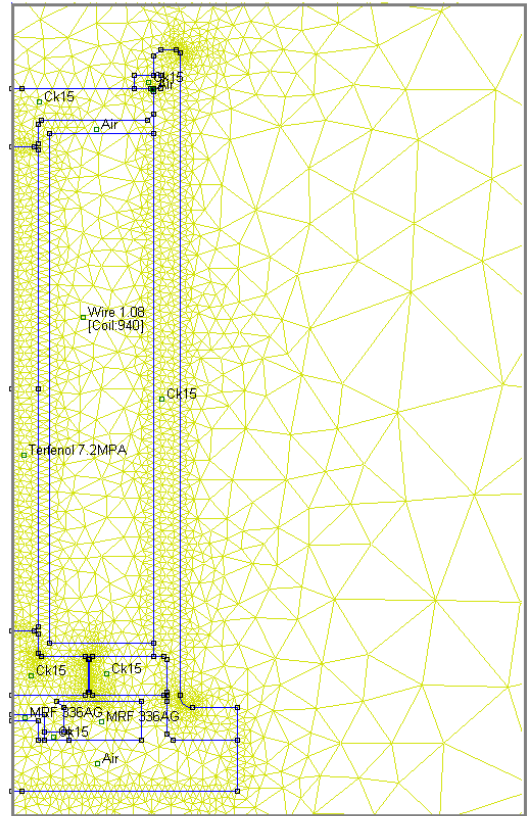
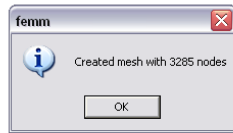
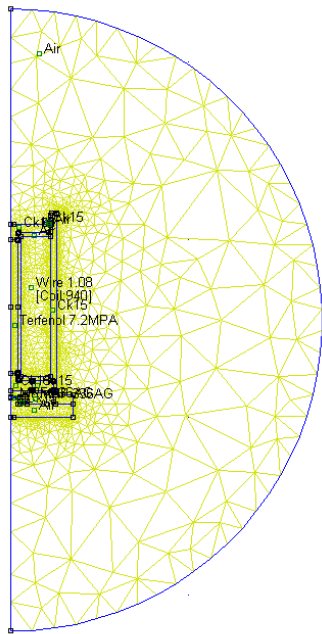
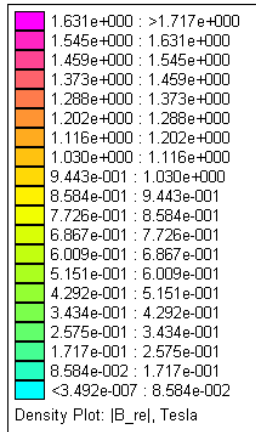
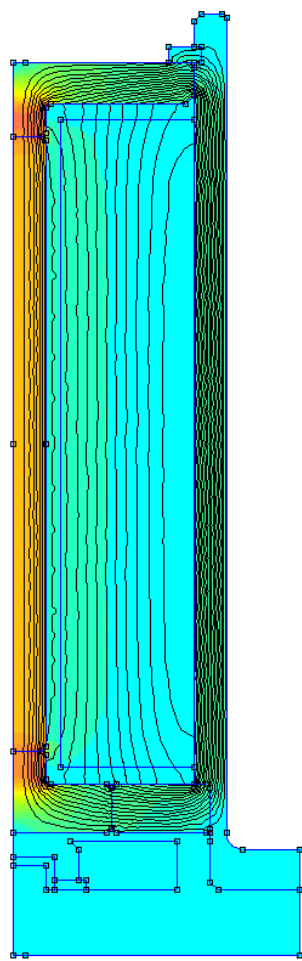


Fig. 17: Meshed actuator with FEMM



Title: 700.000
 Length Units: Millimeters
 Axisymmetric Solution
 3285 Nodes
 6389 Elements

Results	Frequency: 0 Hz
Total current = 9 Amps	
Voltage Drop = 13.6809 Volts	
Flux Linkage = 0.0694634 Webers	
Flux/Current = 0.00994037 Henries	
Voltage/Current = 1.54232 Ohms	
Power = 124.926 Watts	
Results	Frequency: 10 Hz
Total current = 9 Amps	
Voltage Drop = 13.8815 + j6.10813 Volts	
Flux Linkage = 0.0972139 - j 8.75019e-006 Webers	
Flux/Current = 0.0108015 - j 9.72243e-007 Henries	
Voltage/Current = 1.54238 + j 0.678681 Ohms	
Real Power = 62.4666 Watts	
Reactive Power = 27.4866 VA	
Apparent Power = 68.2465 VA	
Results	Frequency: 50 Hz
Total current = 9 Amps	
Voltage Drop = 13.8947 + j30.5406 Volts	
Flux Linkage = 0.0972138 - j 4.37508e-005 Webers	
Flux/Current = 0.0108015 - j 4.8612e-006 Henries	
Voltage/Current = 1.54395 + j 3.3934 Ohms	
Real Power = 62.526 Watts	
Reactive Power = 137.433 VA	
Apparent Power = 150.988 VA	
Results	Frequency: 250 Hz
Total current = 9 Amps	
Voltage Drop = 14.2246 + j152.701 Volts	
Flux Linkage = 0.0972122 - j 0.000218742 Webers	
Flux/Current = 0.0108014 - j 2.43046e-005 Henries	
Voltage/Current = 1.58051 + j16.9667 Ohms	
Real Power = 64.0108 Watts	
Reactive Power = 687.152 VA	
Apparent Power = 690.127 VA	
Results	Frequency: 500 Hz
Total current = 9 Amps	
Voltage Drop = 15.2555 + j305.385 Volts	
Flux Linkage = 0.0972072 - j 0.000437405 Webers	
Flux/Current = 0.0108008 - j 4.86006e-005 Henries	
Voltage/Current = 1.69506 + j 33.9317 Ohms	
Real Power = 68.6499 Watts	
Reactive Power = 1374.23 VA	
Apparent Power = 1375.95 VA	
Results	Frequency: 1000 Hz
Total current = 9 Amps	
Voltage Drop = 19.3755 + j610.644 Volts	
Flux Linkage = 0.097187 - j 0.000874185 Webers	
Flux/Current = 0.0107986 - j 9.71317e-005 Henries	
Voltage/Current = 2.15283 + j67.8493 Ohms	
Real Power = 87.1896 Watts	
Reactive Power = 2747.9 VA	
Apparent Power = 2749.28 VA	

Fig. 18: FEMM Magnetic Field Density plot B (Tesla) in the actuator

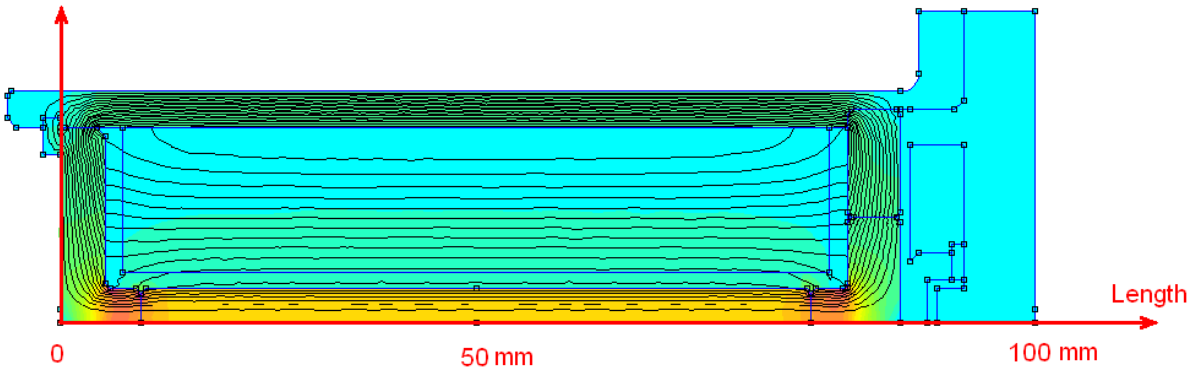


Fig. 19: Reference figure of the actuator plots of B (Tesla) and H (A/m)

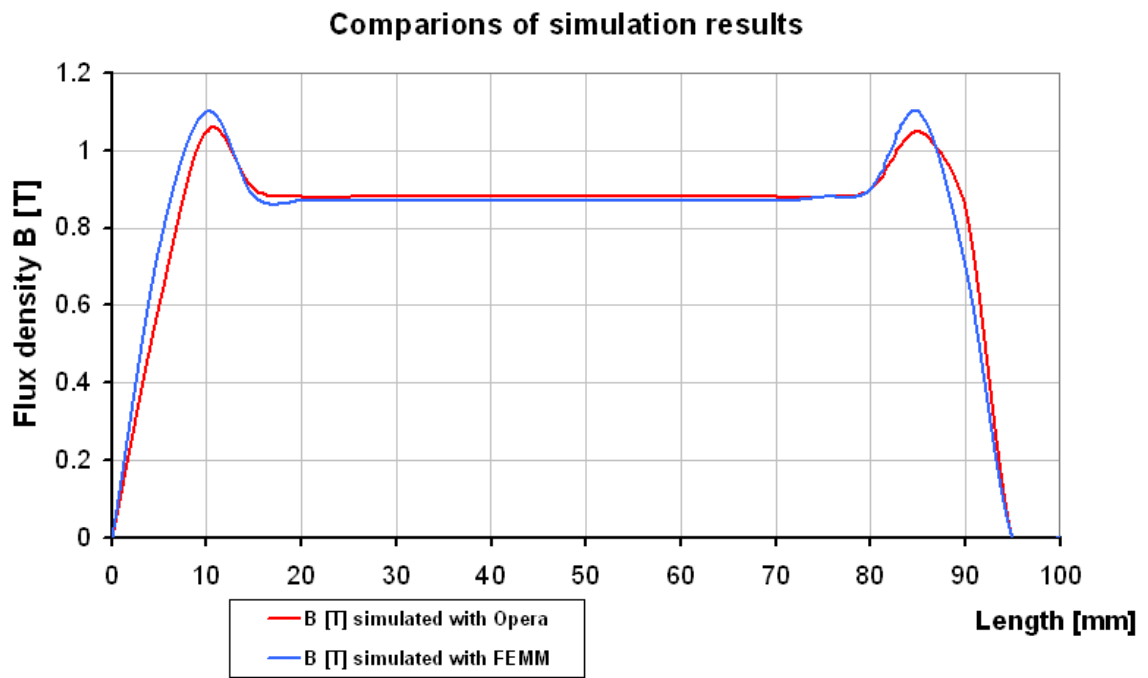


Fig. 20: Comparison of simulation results regarding flux density B (T)

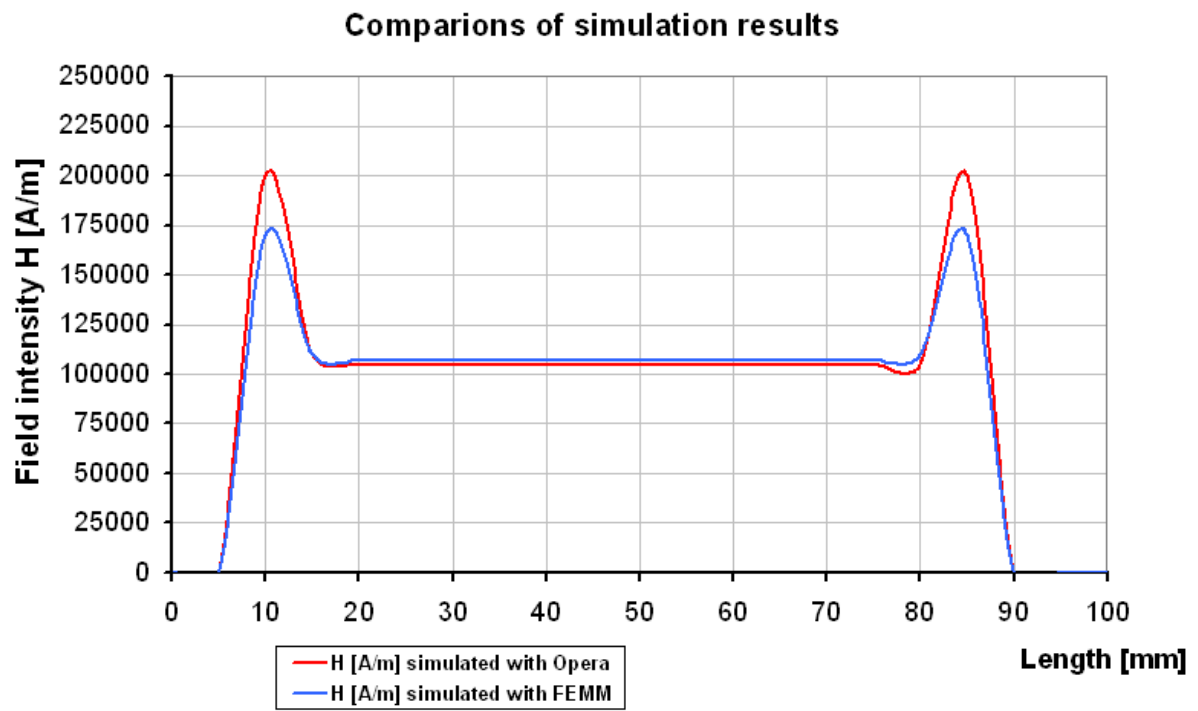


Fig. 21: Comparison of simulation results regarding field intensity H (A/m)

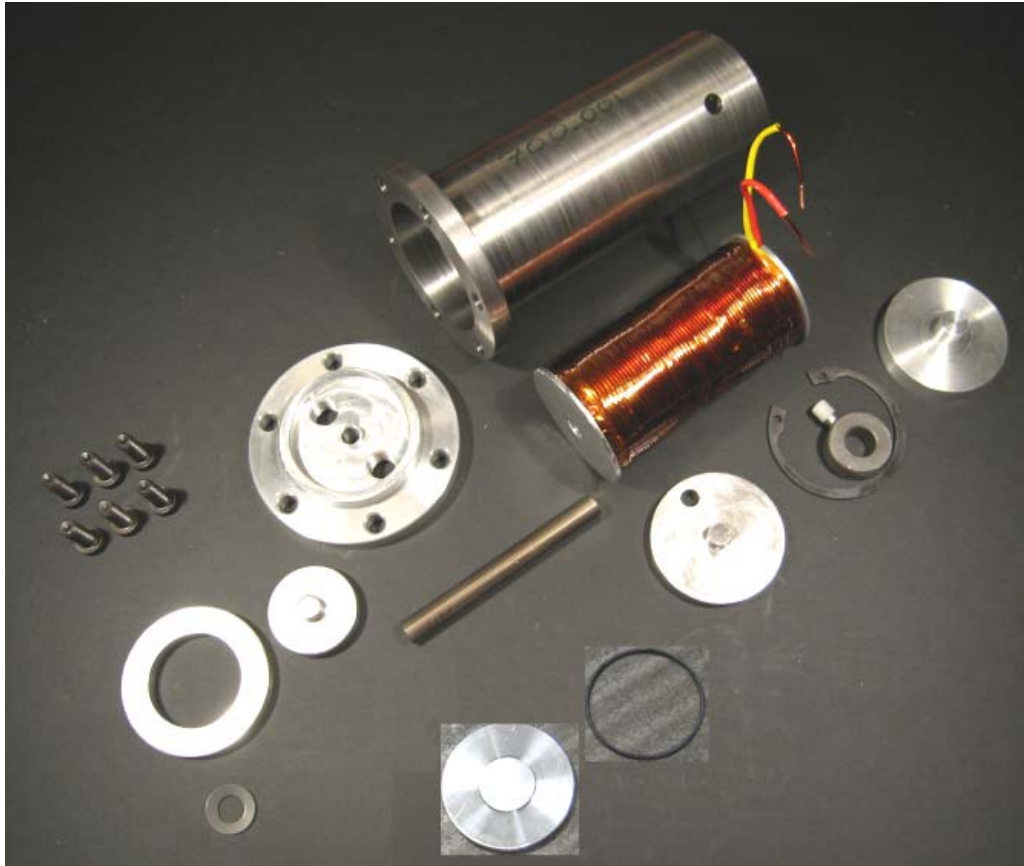


Fig. 22: Picture from “MS”-actuator assembly

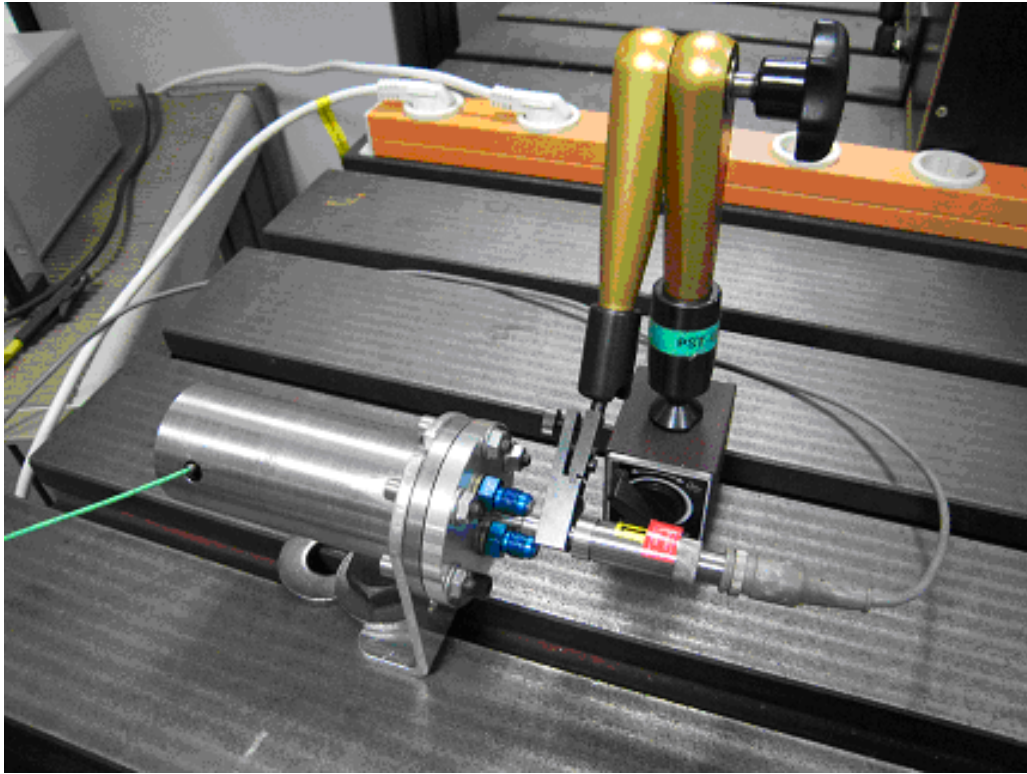


Fig. 23: Actuator assembly for performance measurements

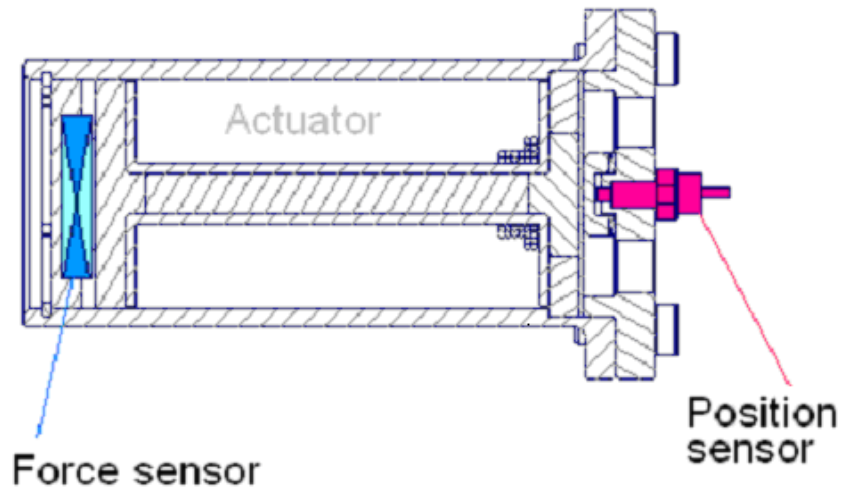


Fig. 24: Actuator assembly cross section for performance measurements

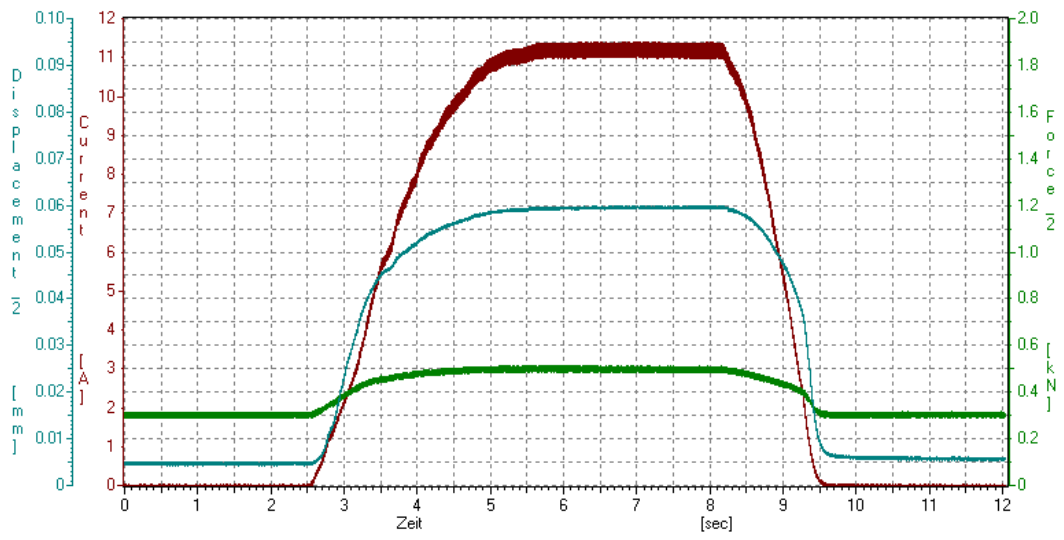


Fig. 25: Displacement, current and axial force versus time with 300 N pre-load

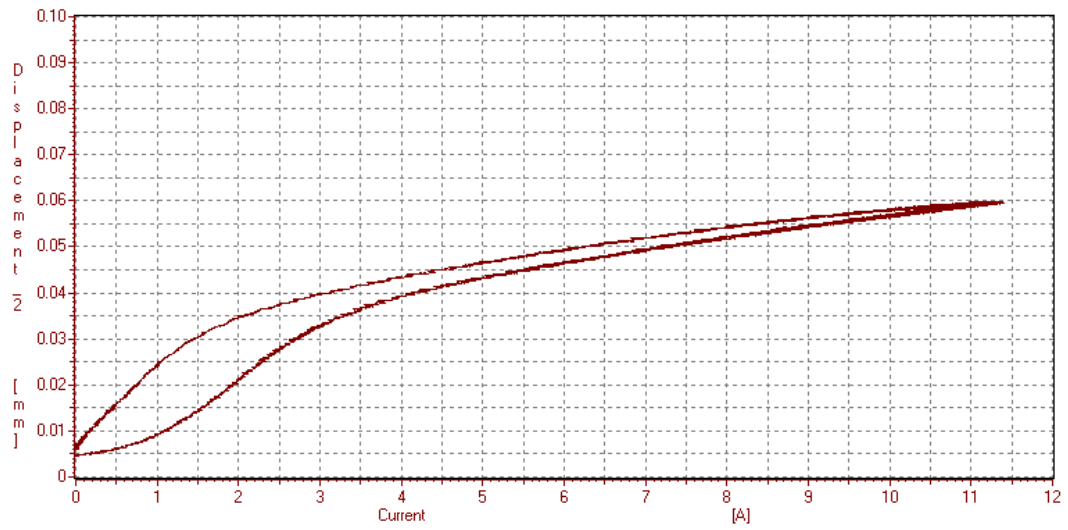


Fig. 26: Displacement versus current with 300 N

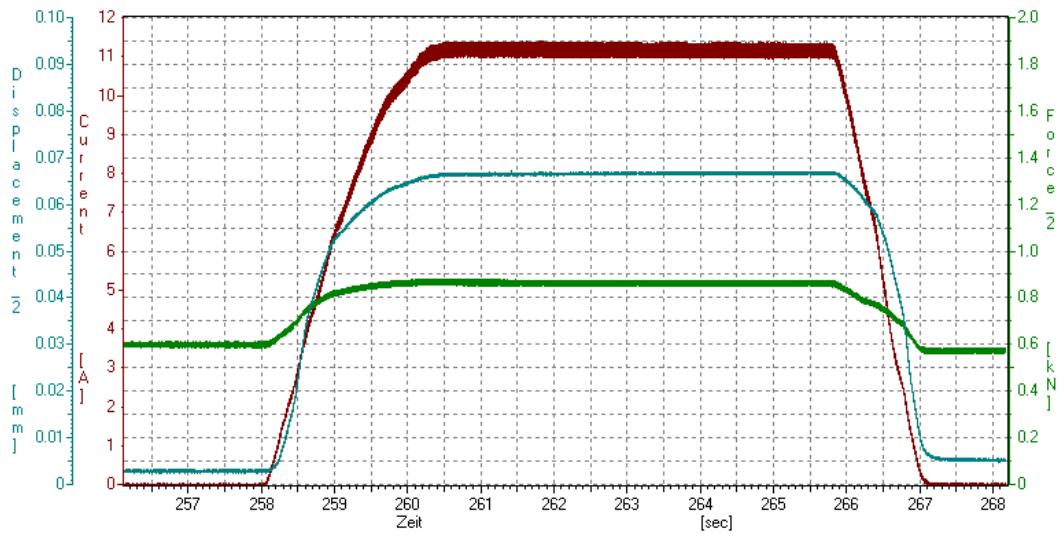


Fig. 27: Displacement, current and axial force versus time with 600 N pre-load

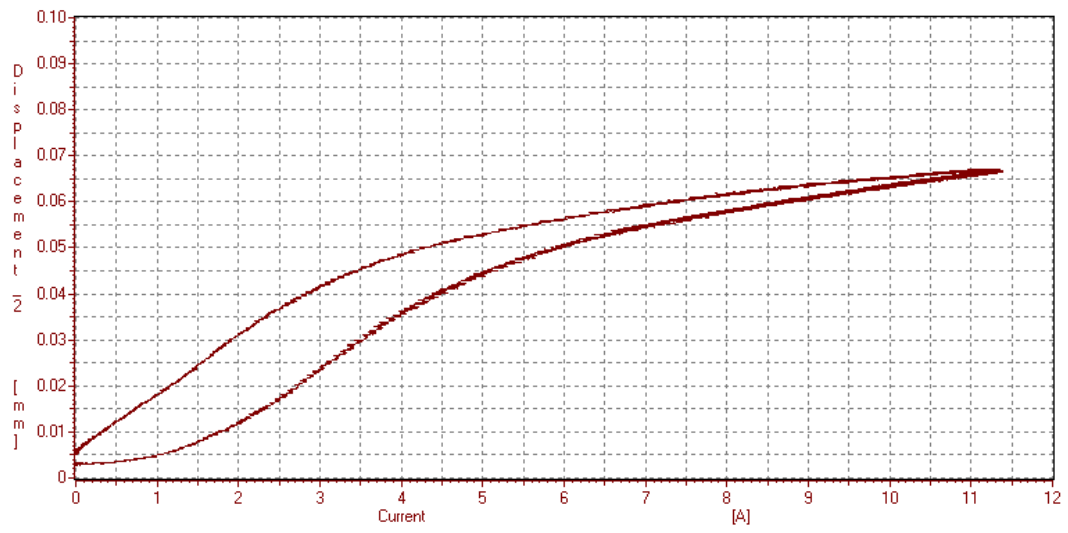


Fig. 28: Displacement versus current with 600 N

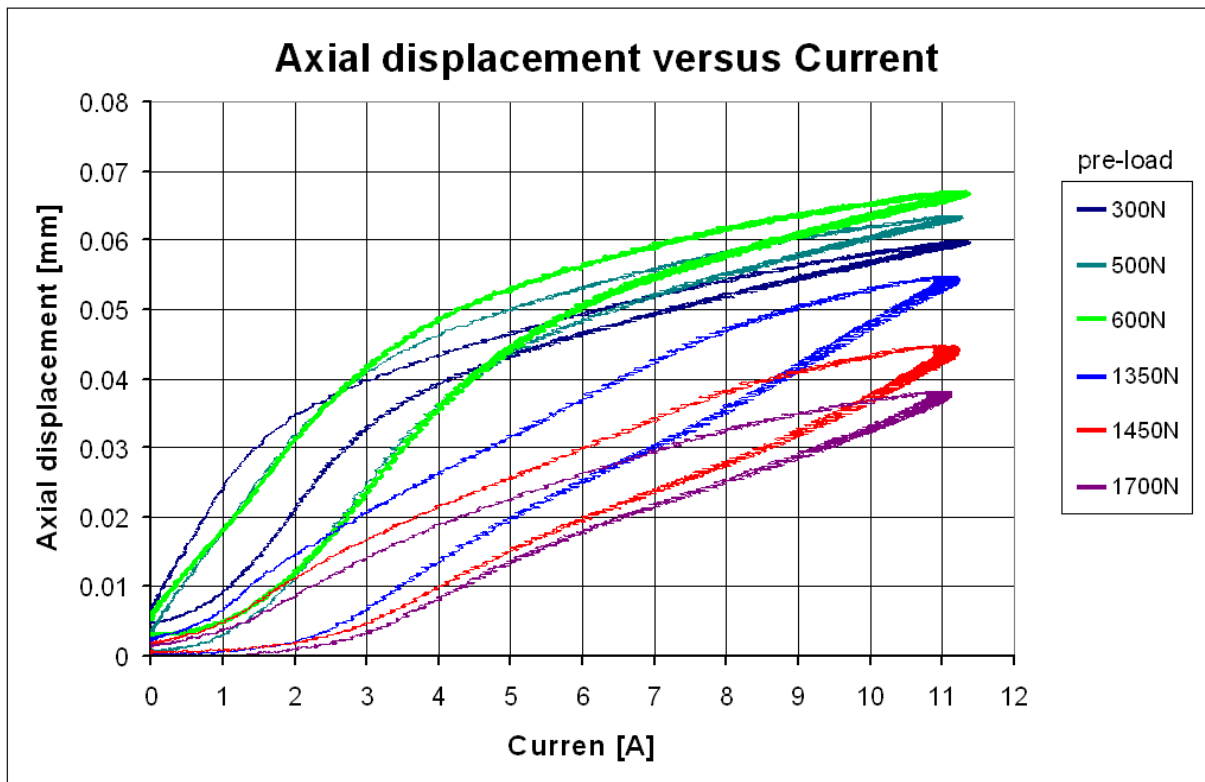


Fig. 29: Optimization of achievable strain with various pre-load

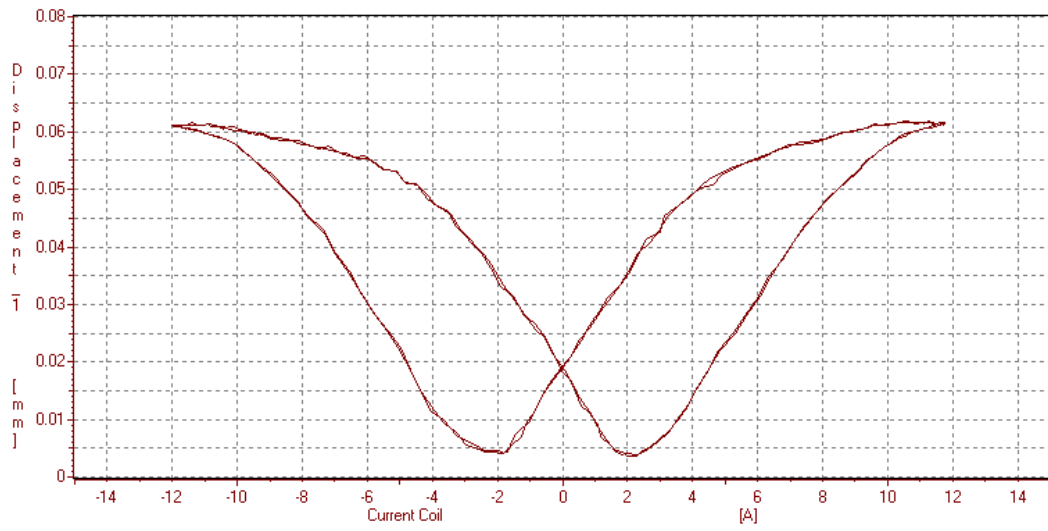


Fig. 30: Butterfly-curve at 550N pre-load & 20Hz sinusoidal power input

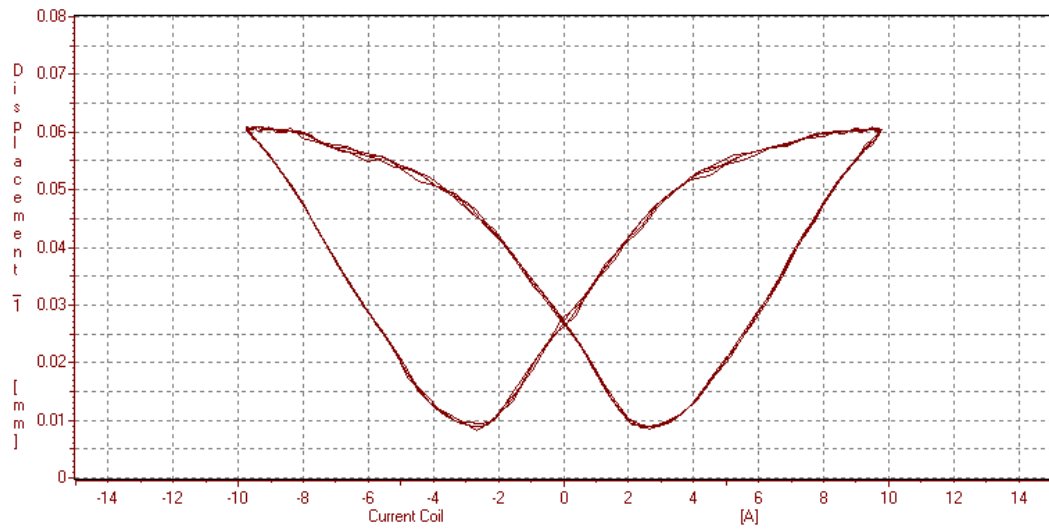


Fig. 31: Butterfly-curve at 550N pre-load & at 40Hz sinusoidal power input

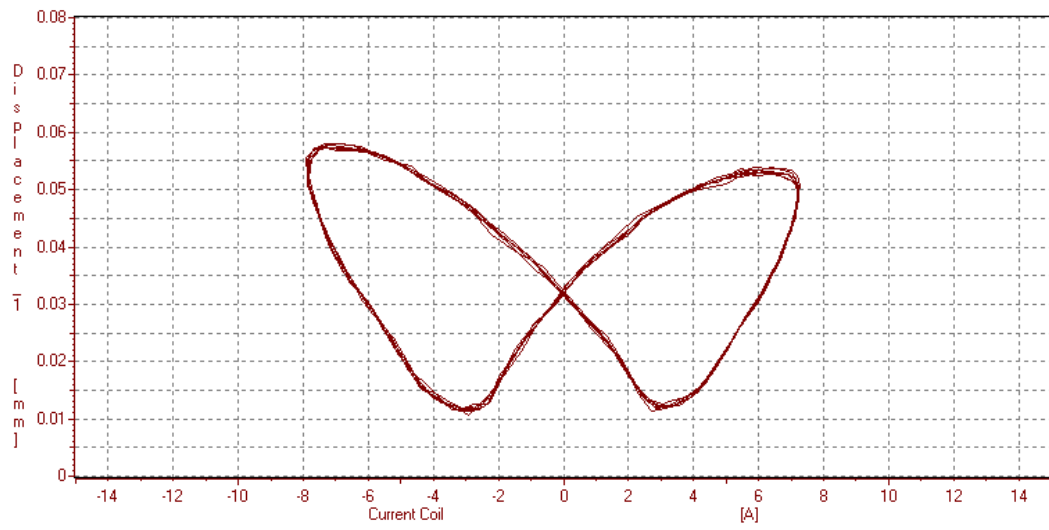


Fig. 32: Butterfly-curve at 550N pre-load & at 60Hz sinusoidal power input

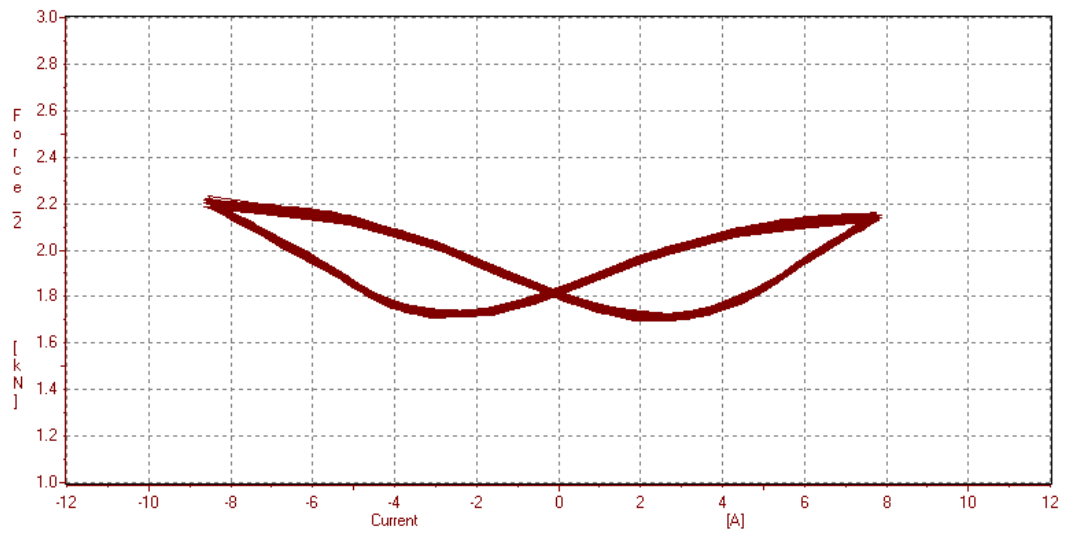


Fig. 33: Butterfly-curves, force versus current at medium pre-stress

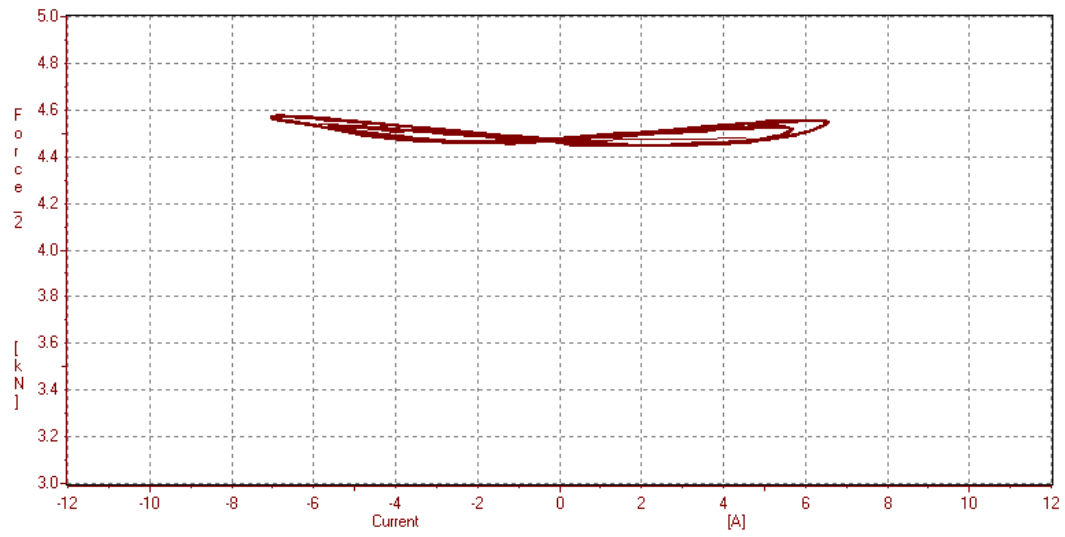


Fig. 34: Butterfly-curves, force versus current, at high pre-stress